

**Exam CT4150 Plasticity Theory**

Wednesday 9 June 2004, 9:00 – 12:00 hours

**Problem 1**

A frame consists of two columns and a roof beam (Figure 1). The left hand column is rigidly connected to the roof beam and the foundation. The right hand column is connected with hinges to the roof beam and the foundation. The frame is loaded by five forces  $\lambda F$ . The columns and beam have different yield contours (Figure 2). The following relation exists between the plastic moment  $M_p$  and the plastic normal force  $N_p$ .

$$N_p = \beta \frac{M_p}{a}$$

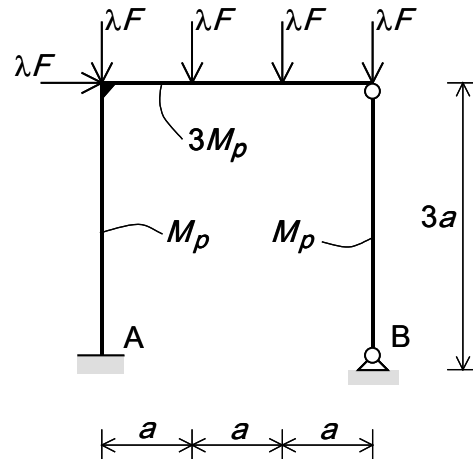


Figure 1. Frame

The influence of shear on the yield contour is neglected. Buckling and second order effects are not considered.

- a** Assume  $\beta \rightarrow \infty$ . Determine the collapse load  $\lambda F$  for every possible mechanism. Write the collapse loads as functions of  $M_p$  and  $a$ . Which mechanism is decisive? What is the corresponding collapse load? (1.5 points)
- b** Assume  $\beta \rightarrow \infty$ . Draw the bending moment and normal force diagram for the whole structure at the moment of collapse (1 point).
- c** Assume  $\beta = 2$ . Choose one of the following problems (You need not do both). Use the decisive mechanism of problem **1a** (2.5 points).
  - Determine the largest lower-bound for  $\lambda F$ .
  - Determine the smallest upper-bound for  $\lambda F$ .

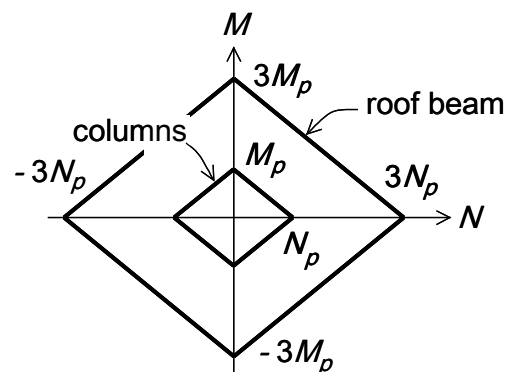


Figure 2. Yield contour

## Problem 2

A square plate is simply supported at parts of the edges (Figure 3). One edge of the plate carries a evenly distributed load  $\lambda f$  [kN/m]. The plate is homogeneous. The yield moment in the  $x$  direction is  $m_p$ . The yield moment in the  $y$  direction is  $3 m_p$  [kNm/m].

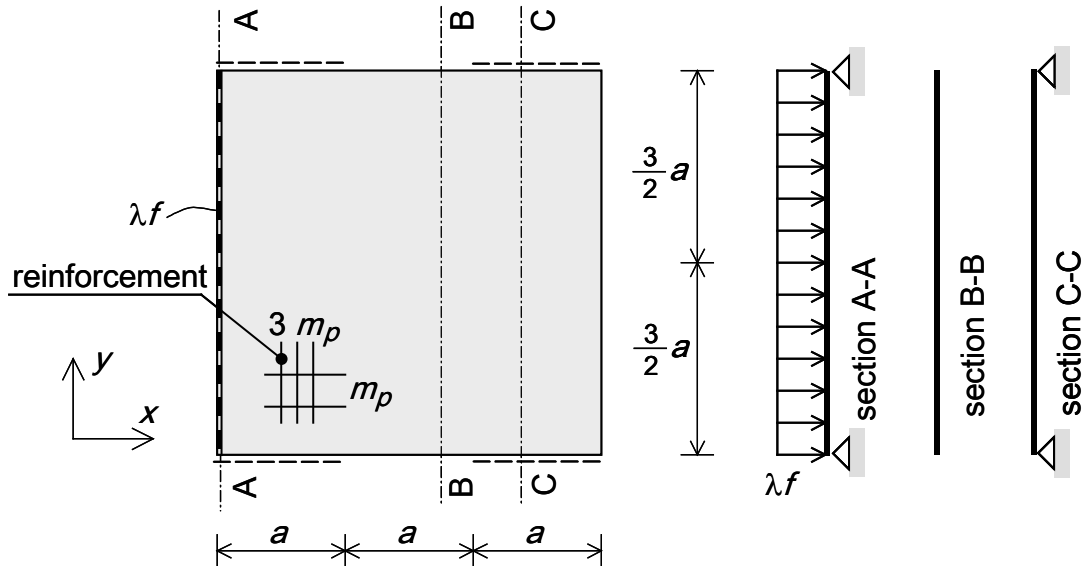


Figure 3. Simply supported square plate

- a We consider the yield line patterns of Figure 4 and Figure 5. Which of these patterns give kinematically possible mechanisms (2 points).

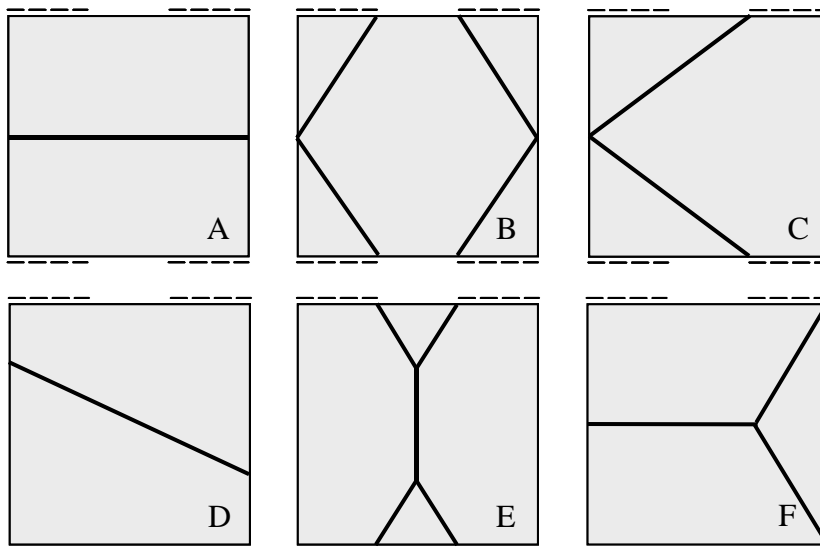


Figure 4. Yield line patterns of problem 2a (see also Figure 5)

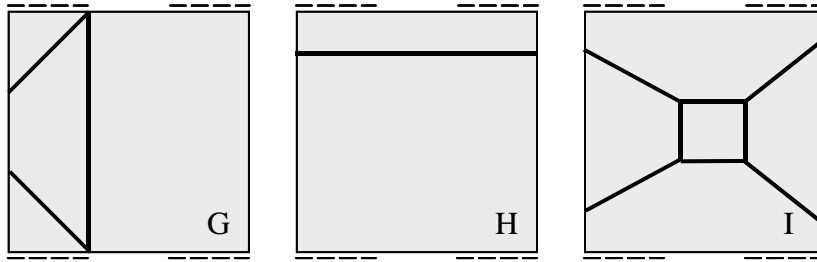


Figure 5. Yield line patterns of problem 2a

- b** We consider the yield line pattern of Figure 6. Determine an upper bound for  $\lambda f$  expressed in  $m_p$  and  $a$  (1 point).

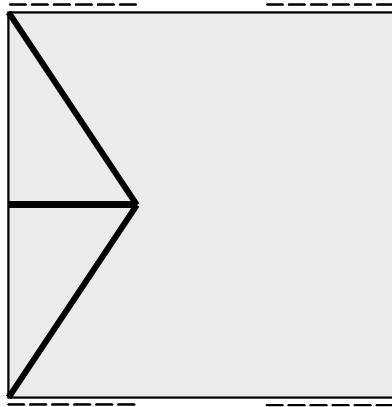


Figure 6. Yield line pattern of problem 2b

- c** Determine the largest lower-bound for  $\lambda f$  using torsion free beams ( $m_{xy} = 0$ ) in the  $x$  direction and  $y$  direction (2 points).

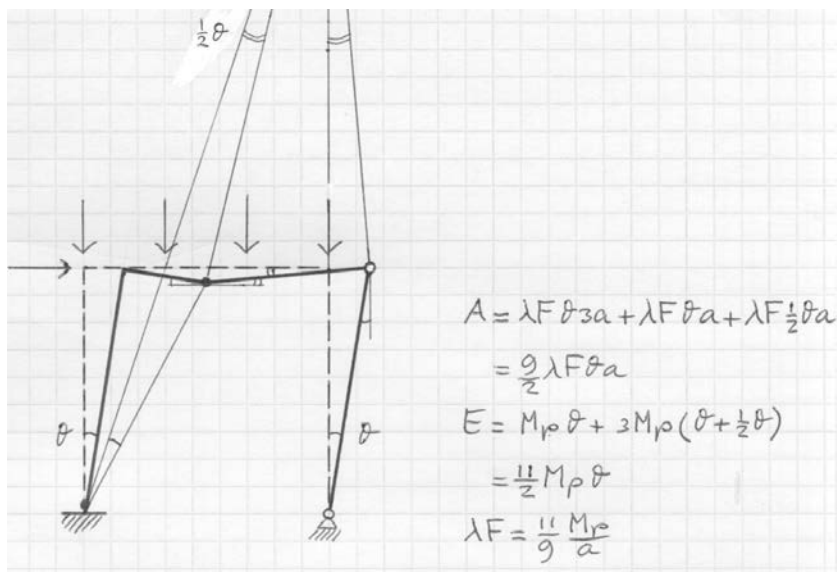
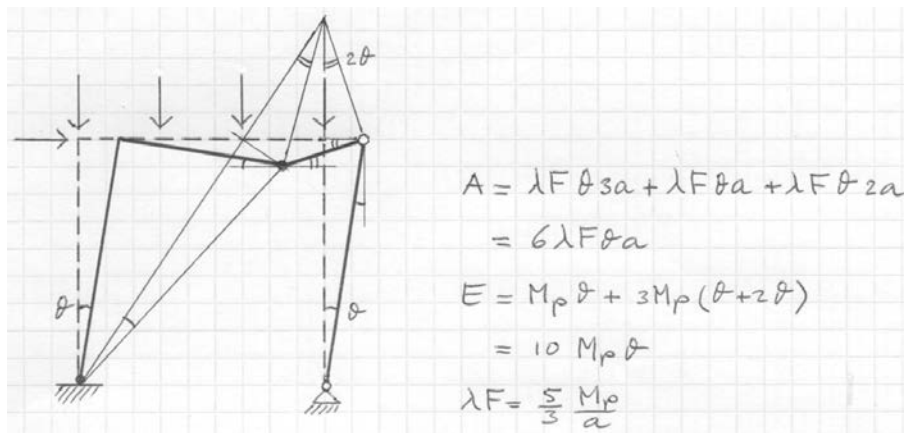
# Answer to Problem 1a

$A = \lambda F \theta a + \lambda F \theta 2a$   
 $= 3 \lambda F \theta a$   
 $E = M_p \theta + 3 M_p (\theta + 2\theta)$   
 $= 10 M_p \theta$   
 $\lambda F = \frac{10}{3} \frac{M_p}{a}$

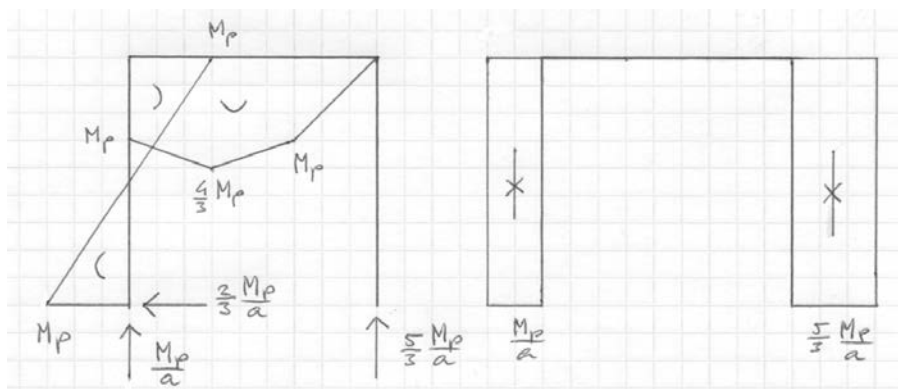
$A = \lambda F 2\theta a + \lambda F \theta a$   
 $= 3 \lambda F \theta a$   
 $E = M_p 2\theta + 3 M_p (2\theta + \theta)$   
 $= 11 M_p \theta$   
 $\lambda F = \frac{11}{3} \frac{M_p}{a}$

$A = \lambda F \theta a$   
 $E = 3 M_p (\theta + \theta) + 3 M_p \theta$   
 $\lambda F = 9 \frac{M_p}{a}$

$A = \lambda F \theta 3a$   
 $E = M_p \theta + M_p \theta$   
 $\lambda F = \frac{2}{3} \frac{M_p}{a} \quad \text{decisive}$



### Answer to Problem 1b



### Answer to problem 1c Lower-bound

We reduce the loading with a factor  $\alpha$ . Also the moments and the normal forces are reduced with  $\alpha$ . In a section with a moment  $\alpha M_p$  we can allow a normal force  $(1 - \alpha) N_p$ . Therefore, at the bottom and top of the left hand column we have

$$N = \alpha \frac{M_p}{a} = (1 - \alpha) N_p = (1 - \alpha) \beta \frac{M_p}{a}.$$

Consequently,

$$\alpha = (1 - \alpha) \beta$$

and

$$\alpha = \frac{\beta}{1 + \beta}.$$

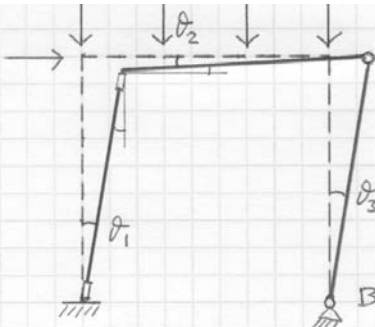
Since  $\beta = 2$  we find

$$\alpha = \frac{2}{3}.$$

The collapse load is

$$\lambda F = \alpha \frac{2}{3} \frac{M_p}{a} = \frac{4}{9} \frac{M_p}{a}$$

### Answer to Problem 1c Upper-bound



$u = \theta_3 \frac{a}{2}$

horizontal displacement of point B  $\rightarrow$

$$\theta_1 3a - \theta_3 3a = 0$$

vertical displacement of point B  $\downarrow$

$$\theta_1 \frac{a}{2} + (\theta_1 + \theta_2) \frac{a}{2} - \theta_3 3a = 0$$

$$\begin{cases} \theta_1 = \theta_3 \\ \theta_2 = \frac{2}{7} \theta_3 \end{cases}$$

$$A = \lambda F \theta_1 3a + \lambda F \theta_2 3a + \lambda F \theta_3 2a + \lambda F \theta_3 a$$

$$= \frac{27}{5} \lambda F \theta_3 a$$

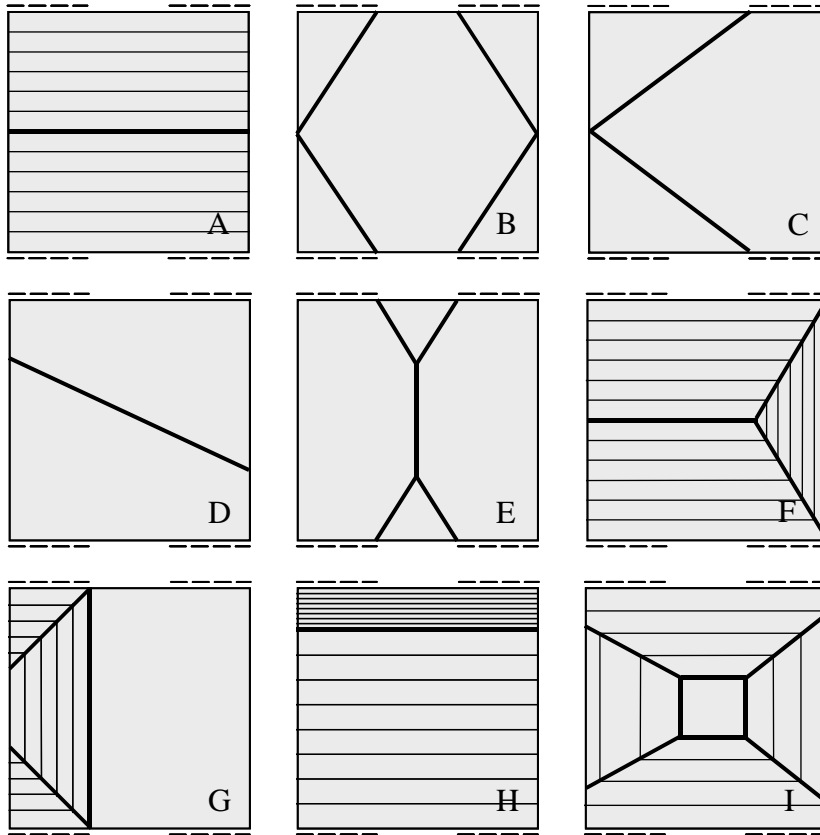
$$E = M_p \theta_1 + M_p (\theta_1 + \theta_2)$$

$$= \frac{12}{5} M_p \theta_3$$

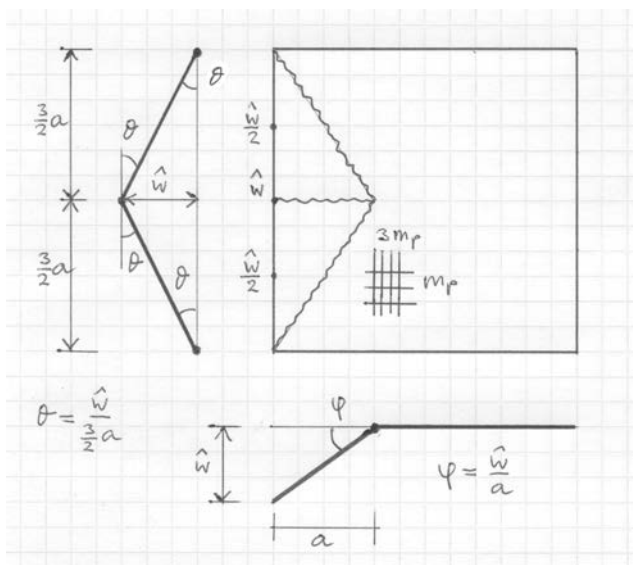
$$\lambda F = \frac{4}{9} \frac{M_p}{a}$$

### Answer to Problem 2a

Kinematically possible are patterns A, F, G, H and I. The figure below shows the altitude lines of the deformed mechanisms.

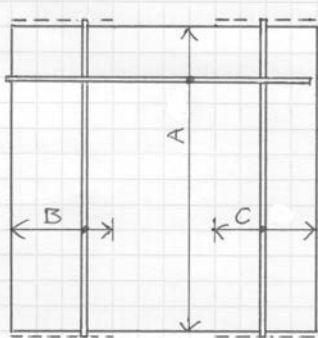


### Answer to Problem 2b

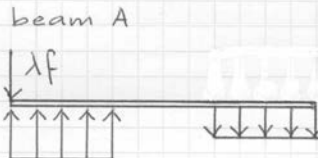


$$\begin{aligned}
 E &= 3m_p a \dot{\theta} + 3m_p a \dot{\theta} + 3m_p a \dot{\theta} + m_p \frac{3}{2} a \dot{\varphi} + m_p \frac{3}{2} a \dot{\varphi} \\
 &= 12 m_p a \dot{\theta} + 3 m_p a \dot{\varphi} \\
 &= 12 m_p a \frac{\hat{w}}{\frac{3}{2}a} + 3 m_p a \frac{\hat{w}}{a} = 11 m_p \hat{w} \\
 A &= \lambda f \frac{3}{2} a \frac{\hat{w}}{2} + \lambda f \frac{3}{2} a \frac{\hat{w}}{2} = \lambda f a \hat{w} \frac{3}{2} \\
 \lambda f &= \frac{22}{3} \frac{m_p}{a}
 \end{aligned}$$

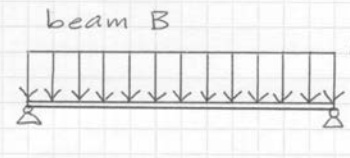
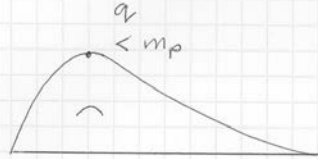
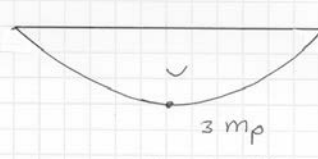
### Answer to Problem 2c



beam A



beam B

$$3 m_p = \frac{1}{8} q (3a)^2$$

$$q = \frac{8}{3} \frac{m_p}{a^2}$$

vert. equilibrium

$$\lambda f - q a + p a = 0$$

mom. equilibrium

$$p a \frac{3}{2} a - q a \frac{1}{2} a = 0$$

$$\left. \begin{aligned} \lambda f - q a + p a &= 0 \\ p a \frac{3}{2} a - q a \frac{1}{2} a &= 0 \end{aligned} \right\} \begin{aligned} \lambda f &= q a - p a \\ p a &= \frac{1}{3} q a \end{aligned} \right\} \lambda f = \frac{4}{5} q a = \frac{4}{5} \frac{8}{3} \frac{m_p}{a^2} a$$

$$\lambda f = \frac{32}{15} \frac{m_p}{a}$$

check

$$\begin{aligned}
 m &= b \lambda f - q b \frac{1}{2} b \\
 &= \frac{\lambda f^2}{q} - \frac{1}{2} q \left( \frac{\lambda f}{q} \right)^2 \\
 &= \frac{1}{2} \frac{\lambda f^2}{q} = \frac{1}{2} \frac{\left( \frac{32}{15} \frac{m_p}{a} \right)^2}{\frac{8}{3} \frac{m_p}{a^2}} = \frac{64}{75} m_p < m_p \text{ okay}
 \end{aligned}$$